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THE 16 APRIL 2015 MW6.1 EARTHQUAKE SEQUENCE NEAR KASOS ISLAND AT THE EASTERN HELLENIC SUBDUCTION ZONE

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Abstract

Broad band seismic waveforms are used to determine the source model of the 16 April 2015 (UTC 18:07:44) earthquake, Mw6.1, which occurred 14 km SW of Kasos Island, in the eastern Hellenic subduction zone. The mainshock is connected with oblique leftlateral motion on a reverse fault, dipping to SE. Most of the aftershocks are compatible with strike-slip or oblique normal faulting, with the T-axes showing along arc extension. A finite fault slip inversion was performed, allowing for the rake angle to vary across the fault, to capture the variation in the slip vectors. The rupture initiated in the lower crust, at a centroid depth of 23 km, and propagated mainly towards SW. The slip is confined in depth within \sim 17km and 27km, mainly in a single asperity, with the peak slip of the order of 60 cm. The slip model provided synthetic seismograms which matched satisfactory the observed, and with forward modelling the ShakeMap was calculated. The 2015 Kasos earthquake sequence is compatible with shear motions parallel to the strike of the subduction zone. It provides evidence that part of the deformation in the eastern Hellenic subduction is taken up by the simultaneous operation of reverse faulting and of minor strike-slip and oblique normal faulting, with slip vectors aligned ~ parallel to the Pliny and Strabo Trenches and the long axis of the local bathymetry.

Keywords: earthquake, slip model, focal mechanism, Hellenic trench.

Περίληψη

Μελετάται η ακολουθία του σεισμού της 16ης Απριλίου (UTC 18:07:44; Mw6.1) που συνέβη ΝΔ της Κάσου. Ο μηχανισμός γένεσης του κύριου σεισμού δείχνει την ενεργοποίηση ενός ανάστροφου ρήγματος, με κλίση προς τα ΝΑ, ενώ των περισσότερων μετασεισμών σχετίζονται με ρήγματα οριζόντιας μετατόπισης ή πλαγιο-κανονικά με αριστερόστροφη οριζόντια συνιστώσα. Η διάρρηζη ζεκίνησε στον κατώτερο φλοιό και διαδόθηκε κυρίως προς τα ΝΔ, προς την Κρήτη. Η ολίσθηση κατανέμεται σε βάθη από 17-27κμ σε ένα κυρίως κλείθρο με μέγιστη τιμή ~60cm. Με ευθύ υπολογισμό υπολογίσθηκε η κατανομή της ταχύτητας στο κοντινό πεδίο, ενώ από εμπειρικές σχέσεις προέκυψε και η κατανομή της μέγιστης επιτάχυνσης, για σύγκριση με τις τιμές που καταγράφηκαν στους επιταχυνσιογράφους. Ο σεισμός της Κάσου καταδεικνύει ότι τμήμα της παραμόρφωσης στην ανατολική περιοχή του ελληνικού τόζου, καταναλώνεται μέσω της δράσης τόσο ανάστροφων ρηγμάτων, όσο και ρηγμάτων οριζόντιας μετάθεσης, με αριστερόστροφη συνιστώσα, των οποίων τα διανύσματα ολίσθησης είναι σχεδόν παράλληλα με την τοπική βαθυμετρία και τις τάφρους. **Λέξεις κλειδιά:** σεισμός, ολίσθηση, μηχανισμός γένεσης, Ελληνικό Τόζο.

1. Introduction

The Eastern Mediterranean active tectonics are mainly controlled by the convergence between Nubia (Africa) and Eurasia at less than 10mm/yr and the rapid movement of southern Aegean southwards, away from Eurasia, at ~30 mm/yr. In this framework, the front part of the Nubia lithosphere, the Mediterranean seafloor, subducts rapidly (~40 mm/yr) beneath the Aegean, forming the well-known Hellenic Subduction Zone. The subduction zone is overlain by a thick (~10 km) pile of sediments which form an accretionary prism, known as the Mediterranean Ridge (see Kiratzi, 2014 and references therein). The bathymetry from Peloponnese, to south of Crete and up to Rodos, is dominated by a number of trenches, the Hellenic Trench dominating in the west, between Peloponnese and western Crete (Fig. 1).





The Hellenic Trench does not mark the actual interface of contact between the down going Nubia lithosphere and the overriding Aegean lithosphere. This interface is marked by the occurrence of earthquakes compatible with low angle thrust mechanisms, dipping towards the overriding Aegean plate. Evidently, these shallow-dipping planes project beneath the pile of sediments, south of Crete. Taking into account the large thickness of these sediments it is very doubtful whether the interface reaches the surface, and more probably it is hidden beneath the sediments, in the form of a blind thrust (Shaw, 2012). The overriding Aegean plate mainly encompasses along-arc E-W extension. This type of normal faulting is widespread in southern Aegean, that is south of the volcanic arc, and

is also evident within the mainland of Crete Island. The subducting Nubia lithosphere undergoes along arc compression, as revealed by the distribution of the focal mechanisms of intermediate depth (h>40 km) earthquakes (Taymaz *et al.*, 1991). Apart from the low-angle thrust and reverse focal mechanisms, which are the signature of the Africa – Eurasia convergence, along the subduction zone strike-slip focal mechanisms are also observed, which are not clearly connected with the interface or the subducting slab. Here, we mainly focus on the reverse and strike-slip faulting on the eastern section of the subduction zone, where the 16 April 2015 (Mw6.0-6.1) earthquake sequence occurred, near Kasos Island. We study the focal mechanism of the mainshock and of its strongest aftershocks, and calculate a finite-fault slip model for the mainshock, in an attempt to better understand the deformation pattern along the eastern subduction zone. The instrumentally recorded seismicity along the subduction zone is rather moderate in size, and the kinematics along this part of the subduction zone are still poorly understood.

2. Characteristics of the 2015 Kasos sequence

2.1 Teleseismic body waveform modelling of the mainshock

The MT5 code (McCaffrey et al., 1991; Zwick et al., 1994) was used to jointly invert the P and SH waveforms, and solve for the strike, dip, rake, centroid depth, seismic moment and source time function, using Green's functions calculated for a point source. For this purpose, broad band GDSN seismograms were downloaded from the Incorporated Research Institutions for Seismology (IRIS) Data Management Centre. The selected stations are in the 30°-80° distance range to avoid complications relating to core phases and shallow velocity structures. The velocity model used was for one layer of 30 km thickness (Vp=6.5 km/s; Vs=3.7 km/s; ρ =2.8 gr/cm³) over a half-space (Vp=8.0 km/s; Vs=4.5 km/s; p=3.3 gr/cm³). A water layer of 1.5 km layer thickness was applied on top of the velocity structure. Prior to the inversion the waveforms were corrected for the instrument response and band pass filtered between 0.01 and 1 Hz. The corrected velocity waveforms were integrated to displacement, and they were re-convolved with the response of the WWSSN 15-100s long period instrument. Finally, the waveforms were decimated at 1s and were cut 20s before and 80s after the phase arrival. 28 P-waves and 17 SH waveforms were finally inverted. The azimuthal coverage is not perfect, and parts of the focal sphere quadrants are not well sampled. This is a common feature with the southern Aegean Sea earthquakes and the geometry of the global stations. The seismograms were weighted according to azimuthal density, and the weights of the SH waveforms were further downscaled to compensate for their generally larger amplitudes. The source time function was parameterized as a series of overlapping isosceles triangles, each having a half duration of 1s. The routine minimizes the weighted squared residuals between observed waveforms and synthetic seismograms computed by combining direct arrivals (P or S) with near-source reflections (pP and sP, or sS). The calculated synthetic waveform amplitudes were corrected for geometrical spreading (Langston and Helmberger, 1975) and for anelastic attenuation using a Futterman Q operator with $t^* = 1.0$ s for P and $t^* = 4.0$ s for SH waves - any uncertainties in t^* have little effect on other source parameters, but mainly result in uncertainties in source duration and seismic moment.

The best fitting solution is summarized in Table 1 and Figure 2. The mechanism shows predominantly reverse motion with a significant component of strike-slip motion, with the centroid depth at 23 km, when the Moho depth in this region is ~26km. The source duration of this model is ~7s. The solution provides an acceptable fit (R/D 75%) between observed and synthetic waveforms in most stations. The uncertainty in the strike of the nodal planes is large (-15°, +0°), whereas for the dip and rake are of the order of \pm 7°, and for the depth is -4, +2 km. From the published solutions for the mainshock (Table 1) our solution is closer to the one determined by NOA-GI. Even though all solutions mostly agree on the centroid depth, there is a large variation, among them, regarding the strike of the nodal planes, which in our modelling as well, the uncertainties regarding the strike, are significant.



Figure 2 - Mechanism of the 2015 Kasos mainshock from the inversion of P and SH body waves. The top focal sphere shows the lower hemisphere projection of the P waveform nodal planes and the positions of the seismic stations used. The lower focal sphere shows the SH nodal planes. Capital letters next to the stations names correspond to the position on the focal sphere. The inversion window is marked with vertical lines in each waveform. Dashed lines represent synthetics and straight lines, observed waveforms. The source time function scale and the waveforms scale are shown at the right corner. The amplitude scale for the waveforms is shown left to each focal sphere.

2.2 Distribution of aftershocks and their focal mechanisms

To calculate the focal mechanisms of the aftershocks the moment tensor inversion technique of Dreger (2002), as described in Roumelioti *et al.* (2011) was applied. The seismic data were broad band velocity waveforms retrieved from the Hellenic Unified Seismic Network (HUSN) and the

Turkish Seismological Network, operated by the Kandilli Observatory. Prior to the inversions, the waveforms were corrected for the instrument response, integrated to displacement, rotated to transverse and radial components, band-pass filtered, and resampled at 1 sps. The cut-off frequencies of the filter applied were 0.02 and 0.08 Hz for the mainshock and the strongest aftershocks, while moderate size aftershocks were filtered between 0.05 to 0.08 Hz. Synthetic Green's functions were computed using the frequency-wavenumber integration code developed by Saikia (1994). Both the waveforms and the synthetics were filtered using the same bandwidth selected. Two 1-D velocity models were tested (e.g., Karagianni *et al.*, 2005 and Novotny *et al.*, 2001) in their ability to describe the low frequency content of the recorded broad band waveforms, and in most cases the latter provided better fits.

Figure 3 (top left) shows the location of the mainshock and of the 20150417 UTC 02:05 Mw5.4 strongest aftershock (asterisks), together with the best located aftershocks. The majority of the aftershocks are forming a ~N-S trending cloud between Kasos and western Crete. A number of minor structures east of Karpathos were also activated. Figure 3 (top right) shows the focal mechanisms of the mainshock and of the strongest aftershocks (Table 1), and the cross-section (bottom of the figure) perpendicular to the strike of local bathymetry, clearly shows that the strongest events occurred mainly in the lower crust, and extend in depth from 20 to ~40 km. It is the shallow seismicity that obscures the pattern of the aftershocks, forming the N-S cloud that does not coincide by any of the nodal planes, and shows the activation of smaller-scale shallower structures.

Date	Origin	Lat	Long	h	Mw	NODAL		NODAL			Slip Vector		R	
	Time		_			P	PLANE 1		PLANE 2					
Y/M/D	h:m:s	°N	°E	km		s°	d°	r°	s°	d°	r°	az°	pl°	
20150416	18:07:44	35.23	26.82	23	6.1	75	40	56	296	58	115	26	-32	1
"	"	35.03	26.85	24	6.1	56	43	21	310	76	131	40	-14	2
"	"	35.23	26.82	28	6.0	71	51	68	284	44	115	14	-46	3
20150416	18:52:37	35.17	26.90	22	4.7	233	83	-6	324	84	-173	234	6	1
20150416	19:02:14	35.13	26.85	26	5.0	236	86	5	146	85	176	236	-5	1
"	19:02:18	35.17	26.80	20	5.0	249	71	38	145	55	156	235	-36	2
20150416	20:01:13	35.19	26.75	25	4.1	324	83	-176	234	86	-7	144	4	3
20150416	21:52:24	35.22	26.86	21	4.0	218	68	1	128	89	158	218	-1	3
20150417	01:50:45	35.17	26.74	25	4.1	223	65	-26	325	67	-152	235	23	3
20150417	02:05:42	35.16	26.74	25	5.4	234	71	-35	337	57	-157	247	33	1
"	02:05:44	35.00	26.61	25	5.5	231	77	-40	332	51	-163	242	39	2
20150417	10:23:46	35.20	26.67	28	4.2	239	71	2	148	88	161	238	-2	3
20150417	16:39:41	34.96	26.74	24	4.5	215	81	-9	306	81	-171	216	9	1
20150422	20:19:58	35.29	26.71	28	4.2	222	70	10	129	81	160	219	-9	3
20150427	14:16:32	35.17	26.82	28	4.0	227	26	39	101	74	111	191	-16	3
20150511	05:02:01	35.01	26.90	32	4.5	46	82	2	316	88	172	46	-2	3
20150609	21:49:48	35.07	26.80	24	5.4	236	80	19	143	71	169	233	-19	1

 Table 1 – Source parameters of the mainshock and the strongest aftershocks of the 16 April

 2015 Kasos Island sequence.

Ref (R): 1: this study; 2: GCMT solution; 3: NOA-GI (National Observatory of Athens- Geodynamic Institute).



Figure 3 - top left: Epicentres of the sequence (orange circles) and the location of the mainshock and the strongest aftershock (stars); top right: focal mechanism of the mainshock and of the aftershocks (orange beach balls) together with those from previous strong events (grey beach balls). Oblique normal and strike-slip motions are prevailing in most of the cases whose slip vector is marked with the orange arrow (SV), compatible with left-lateral shear parallel to the trench. The GPS velocity vector shows the motion of the islands relative to Eurasia, which is oblique to the trench; bottom: cross-section along A-B line shows that a) the main sequence is confined at the northern edge of the Pliny Trench and the strongest aftershocks alongside the mainshock occurred below 20 km, in the lower crust, and b) it is the shallower seismicity that obscures the pattern of the ENE-WSW trending fault plane.

From the cross section (Fig. 3) it can be deduced that the mainshock is compatible with reverse faulting that dips to the SE. This is confirmed by the subsequent analysis for the calculation of the slip model, during which the nodal plane which provides statistically significant better fit to the data, can be identified. The ENE trending plane that dips towards SE implies a moderate component of left-lateral strike-slip motion. It must be noted, that the strongest Mw5.4-5.5 aftershock, implies oblique normal faulting and E-W extension, like the one observed within the overriding Aegean plate. The focal depths of all events analysed are around 20-32 km. The average orientation of the slip vectors, for the earthquakes listed in Table 1, is 220°. This orientation is oblique to the local orientation of the GPS velocity vectors (~195°), but is parallel to the strike of the subduction zone and aligns with the long axis of the basin bathymetry (Pliny and Strabo Trenches).

3. Slip Model of the Mainshock

3.1 Method

The slip distribution onto the fault plane is investigated through a linearized least-squares inversion with simultaneous smoothing (e.g., Hartzell and Heaton, 1983; Dreger and Kaverina, 2000; Kaverina et al., 2002) as applied to previous Aegean earthquakes (Kiratzi et al., 2013 and references therein). Extensive resolution and checkerboard tests of the applied method are included in Benetatos et al. (2007). The source has finite dimensions and the fault plane is discretized into a number of subfaults. The rupture is assumed to propagate from the hypocentre with constant rupture speed and each subfault is allowed to rupture only once as the rupture front passes. In our model parameterization, the slip history of each subfault was represented by an appropriate number of isosceles triangles, and moreover, the rake angle was allowed to vary over the fault plane. Synthetic waveforms are finally derived as the result of the summation of the individual subfault contributions, using appropriate time delays for both the time needed for the wave to propagate from the hypocentre to the recording stations and the time needed for the rupture front to propagate from the hypocentre to the centre of each subfault. The applied linearized least-squares inversion is combined with slip positivity, spatial gradient smoothing and moment minimization constraints. The slip positivity constraint implies that slip is allowed to occur only along the rake direction, while the moment minimization constraint reduces spurious slip in the later portions of the rupture.

3.2 Finite-fault slip model

Initial inversion runs indicated that the SE dipping plane provided significant better Variance Reduction (63%) compared to the conjugate nodal plane (44%). Thus the slip model was calculated for the geometry of this plane (Table 1). To capture the variation of slip vectors onto the fault plane, the rake angle was allowed to vary $\pm 45^{\circ}$. The fault plane was discretized into 35×35 square subfaults, of 1×1 km² area, along strike and dip, respectively. The subfaults were sized so that the rupture process is smooth and the transit time across them, taking into account the rupture velocity, is also smooth. The dimensions of the fault model were chosen large enough to allow the slip to find its preferred position. The rise time and the rupture velocity, were grid searched for the optimal values, and were finally adopted equal to 0.5s and 2.7 km/s, respectively. We separately calculated the dipslip and strike-slip components, finally using the vector summation for both components.

Figure 4 summarizes the preferred slip model, in fault coordinates centred at the rupture initiation point at 12 km depth, for the parameterization adopted. Slip is confined within 17 to 27 km depth, mainly in a single asperity. Minor slip is also found in a smaller asperity at southwest, alongside rather unstable spurious shallow slip. The average slip is 9 cm and the peak slip is ~60 cm in accordance with the predictions of empirical scaling relations. The total moment of the model is 1.55e18 N-m, corresponding to Mw6.1, in accordance with the reported values to the European Mediterranean Seismological Centre (EMSC) from the various seismological agencies. The slip model predicts synthetic waveforms that fit the observed ones very satisfactorily as can be seen from the comparison (Fig. 5).



Figure 4 - Slip model for the mainshock, obtained from finite fault inversion, using regional broad band seismic waveforms. The *white* lines denote the variable rake onto the fault plane, and the *red* asterisk marks the rupture initiation point (note that it is at 12 km). The locus of maximum slip (~60cm) is confined within 17 and 27 km in agreement with the centroid depth from the teleseismic modelling.



Figure 5 - Comparison of synthetic waveforms (dashed lines) calculated using the slip model for the mainshock, with the observed ones (straight lines) for all station components included in the slip model inversion.

3.3 ShakeMap from forward modelling

The slip model was used in a forward modelling procedure in order to calculate synthetic velocity records in a grid of nodes covering the broader region. These velocity records were then used to map the spatial variation of ground motions. The mainshock was recorded in a number of accelerographs, located in Kasos, Crete and Karpathos islands (Table 2). The acceleration on the instrument located in a rock site in Zakros (Crete) at a distance of 56 km was 56.0 cm/s². The recording at an alluvium site at the Town Hall on Karpathos island, at a distance of 47 km, was 98.5 cm/s² (Kalogeras and Melis, 2015).

C4 - 4 ¹	Location	Surface	Stat	tion in a tag	Distance	PGA (cm/s ²)			
Station Code	Location	geology	Lat °N Lon °E		km	Ζ	X (E)	Y (N)	
KSS1	Kasos Isl.	n/a	35.4189	26.9209	23	32.1	29.3	43.2	
KRPA	Karpathos	Alluvium	35.5082	27.2092	47	25.6	83.3	98.5	
ZKR	Zakros	limestone	35.1146	26.2171	56	20.0	49.8	56.0	
SIT2	Sitia	n/a	35.2059	26.1070	68	33.0	78.4	60.3	

Table 2 – Recorded PGA's at selected accelerographs located on nearby locations.

The map of Figure 6b compares the distribution of PGA as this is predicted from the empirical scaling relations of Skarlatoudis *et al.* (2003, 2007). The predicted accelerations on the Kasos island are of the order of 60 to 70 cm/s², and overestimate by ~40% the values actually recorded by the KSS1 strong motion instrument. On the other hand, the empirical GMPs seem to accurately predict the values on the limestone site on the ZKR station in Crete. It must be noted here, that all maps presented in Figure 6, have been corrected for the site effect, using the topography gradient, as proxy, for the values of Vs30, following Wald and Allen (2007).



Figure 6 - a) ShakeMap (PGVs in cm/s) of the 2015 mainshock, produced using forward modelling and the slip model (Fig. 4). b) Distribution of PGA in cm/s² using the empirical relations of Skarlatoudis *et al.* (2003, 2007).

4. Summary

The Kasos 2015 earthquake which occurred in the eastern Hellenic subduction zone is connected with rupture of a reverse fault, at 23 km depth, trending ~ ENE-WSW and dipping to the SE. The calculated slip model, using broad band regional waveforms, and finite-fault inversion techniques, shows that the slip was mainly confined in two patches onto the fault plane. This slip model predicts synthetic waveforms that satisfactorily match the observed ones. The ShakeMap calculated from the slip model shows moderate ground shaking, mainly along the southern coast of the island of Kasos, and offshore towards southwest.

The Kasos sequence occurred shoreward of the Pliny Trench at depths that range from 20 to ~40km. The Moho at this region is at ~26km and the thickness of the seismogenic layer is approximately 40 km. The focal mechanism of the mainshock (reverse faulting) implies that the P-axis is trending N164°E. It must be noted that the focal mechanisms of most of the strong aftershocks are compatible with left lateral strike-slip and oblique normal faulting, mainly along ENE-WSW (~50°) trending planes, which implies along arc extension. Within this framework, the GPS obtained velocity vectors (Fig. 1) show that the motion of the Karpathos, Kasos and western Crete relative to Africa is oblique to the strike of the subduction zone, as well as the long axis of the Pliny and Strabo Trenches. This oblique convergence motion implies that a trench-parallel and a trench - perpendicular component is expected. The trench - parallel component is mainly accommodated by the distributed strike-slip and oblique normal faulting earthquakes, as is the case of most aftershocks in these sequence, whose slip vectors are oriented parallel to the trench and imply left-lateral shear at this part of the subduction zone. The trench - perpendicular component is expected to be accommodated by large reverse faults, parallel to the strike of both the subduction zone and to the Pliny and Strabo Trenches. In fact, these trenches in analogy with the Hellenic Trench, may equally well be the surface expressions of large scale reverse faults, which are geometrically required to accommodate part of the deformation. The 2015 Kasos sequence is compatible with trench-parallel shear motions.

5. Data and resources

Digital seismic waveforms were retrieved from the Hellenic Broad Band Seismic Network (NOA: doi:10.7914/SN/HL; AUTH: doi:10.7914/SN/HT; UPSL: doi:10.7914/SN/HP). The catalogues AUTH and NOA were used. Moment tensors were computed using the code developed by Douglas Dreger and Sean Ford of the Berkeley Seismological Laboratory, and Green's functions were computed using the FKRPROG software developed by Chandan Saikia. All figures were produced using the GMT software (Wessel and Smith, 1998). The Earthquake Planning and Protection Organization (EPPO-OASP) is gratefully thanked for partial support of the operation of the AUTh Seismological Network. Nikos Theodoulidis provided the accelerograms from stations KSS1 and SIT2.

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